 POLITECNICO MILANO 1863 Academic year 2022/2023	094784 Fund. of Electromagnetic Fields	Date: _____
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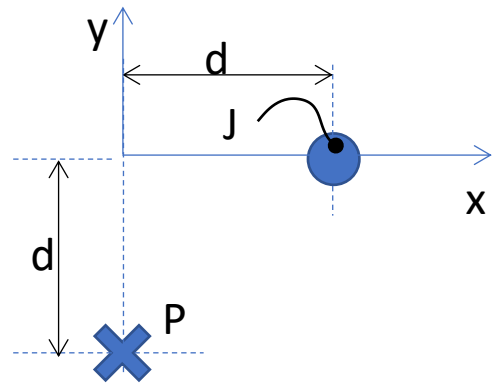
22 June 2023 EXAM


Please answer the following questions/problems, providing a meaningful explanation of the steps/computations involved. Please specify units for all numeric results requiring them, otherwise those results will be considered wrong. Allowed support material: books, notes, scientific calculator.

Exercise 1 [8 points]

A constant (static) uniform volumetric current density $\vec{J} = J \hat{i}_z$ flows along z in an infinite wire of radius $R=2\text{mm}$ placed as in the figure, with $d=15\text{cm}$ in a uniform material. The total magnetic field in the observation point P is: $\vec{H} = (-15\hat{i}_x + 15\hat{i}_y)\text{mA/m}$:

1. derive the expression of the magnetic field outside an infinite wire carrying a uniform volumetric current density J starting from Ampere's law;
2. compute J and the total current I carried by the wire, specifying whether it is toward $+z$ or $-z$.



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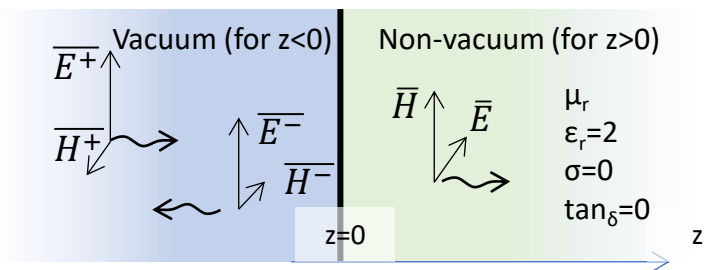
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Exercise 2 [12 pt]

Two plane waves at a frequency of 12GHz counterpropagate in vacuum toward $\pm z$ with the electric field directed along x. The wave propagating toward $+z$ carries a power density $S^+=75.6\text{mW/m}^2$. The wave propagating toward $-z$ instead carries a power density of 8.3mW/m^2 .

- Write the complete expression of the total electric field for $z<0$ as a function of time, assuming the electric fields of the two waves both have phase= 0° in $z=0$ (neglect what happens in $z\geq 0$).
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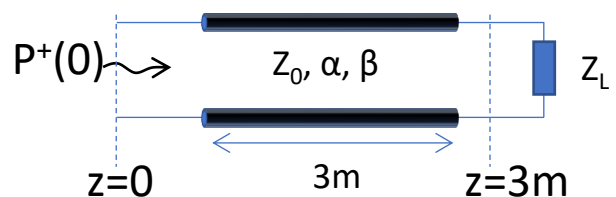
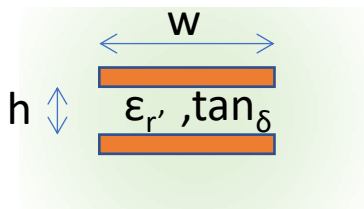
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Exercise 3 [12 pt]

A parallel plate transmission line $w=1\text{cm}$ -wide in a dielectric with $\epsilon_{pr}'=2.75$ (homogeneous) and $\mu_r=1$ has the following parameters per unit length: $L=277\text{nH/m}$, $C=110.4\text{pF/m}$, $R=0\text{Ohm/m}$, $G=0.01\text{S/m}$. At a frequency of 20GHz , under the quasistatic approximation (hence the electrostatic parallel-plate capacitance can be used) and using the low-loss approximation if applicable:

1. Compute the spacing h between the conductors of the line
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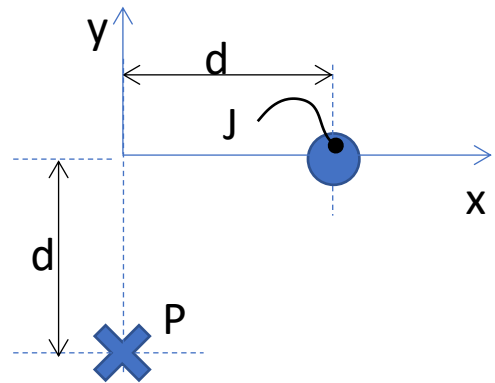
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Solution

The expression of magnetic field due to a single wire can be obtained by circular symmetry:

$\vec{H} = H_\phi(r) \hat{i}_\phi$ as being only directed along the ϕ versor in cylindrical coordinates around the wire's axis and from Ampere's law:

$$\oint_L \vec{H} \cdot d\vec{l} = \iint_{S \text{ enclosed by } L} \vec{J} \cdot d\vec{S}$$

Choosing a circular path of radius $r > R$ and if the uniform current density is parallel to the wire, $H_\phi(r) 2\pi r = J\pi R^2 = I$.

The field from current distribution $\vec{J} = J \hat{i}_z$ creates a field in the observation point which has both

\hat{i}_x and $-\hat{i}_y$ components: $\vec{H}(P) = \frac{I}{2\pi d \sqrt{2}} \hat{i}_{\phi(P)} = \frac{I}{2\pi d \sqrt{2}} \frac{\hat{i}_x - \hat{i}_y}{\sqrt{2}}$ which is obtained by observing that the \vec{H} field is directed at -45° with respect to the x axis.

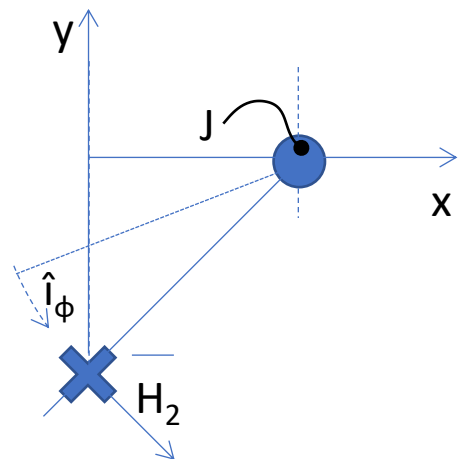
The observed magnetic field exactly fits this form, and equating either the x or y component yields:


$$\frac{I}{2\pi d \sqrt{2}} \frac{1}{\sqrt{2}} = -15 \frac{\text{mA}}{\text{m}} \rightarrow I = -15 \frac{\text{mA}}{\text{m}} 4 \pi d = -28.3 \text{mA}$$

Thus the total current carried by the wire is 28.3mA toward $-z$.

The corresponding uniform volumetric current density has thus a z component given by $I/$ "cross section of wire":

$$J = -28.3 \text{mA} / (\pi R^2) = 2252 \text{A/m}^2$$



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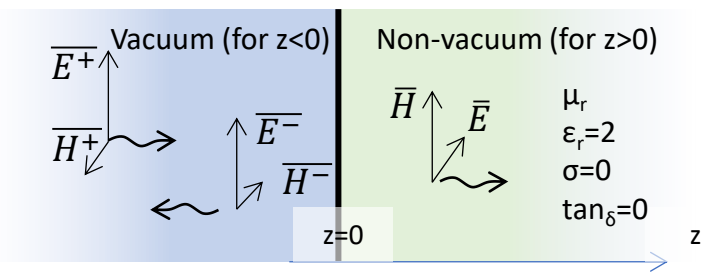
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Solution

A plane wave in a lossless medium (such as vacuum in $z<0$) propagating toward $+z$ with electric field vector E^+ along $+x$ ($E^+=E_x^+ i_x$) must have its magnetic field vector H^+ along $+y$ ($H^+=H_y^+ i_y$), such that the Poynting vector expressing the real power density carried is positive and directed toward $+z$:

$$S^+=0.5 \text{Real}(E^+ \times H^{+*})=0.5 \text{Real}(E_x^+ (H_y^+)^*) i_z=0.5 \text{Real}(E_x^+ (E_x^+)^*/\eta_1)=0.5 |E_x^+|^2/\eta_1$$

Where the last step uses that the magnetic and electric fields are in phase and their magnitudes are governed by the real wave impedance of the material $\eta_1=\text{sqrt}((\mu_0 \mu_{r1})/(\epsilon_0 \epsilon_{r1}))=377 \Omega$ such that $E_x^+/H_y^+=\eta_1$.

Hence the electric field of the $+z$ wave has amplitude $|E_x^+|=7.55\text{V/m}$.

Recalling that the phase of the wave toward $+z$ is 0° , the electric field is:

$$E^+(z)=|E_x^+| i_x e^{j0} e^{jk_1 z} \text{ with } k_1 \text{ the wave number in medium 1: } k_1=\omega \text{ sqrt}(\mu_0 \mu_{r1} \epsilon_0 \epsilon_{r1})=251.5 \text{ rad/m.}$$

The same can be done for the electric field E^- of the wave propagating toward $-z$, although observing that its magnetic field is $H_y^- = H_y^- i_y$ with $E^- = E_x^- i_x$ and $H_y^- = -E_x^-/\eta_1$

Hence the electric field of the $-z$ wave has amplitude $|E_x^-|=2.5\text{V/m}$ and the electric field in vector phasor form is: $E^-(z)=|E_x^-| i_x e^{j0} e^{+jk_1 z}$

The expression of the total electric field as a function of time is thus:


$$\mathcal{E}(z,t)=\text{real}((E^+(z) + E^-(z)) e^{j\omega t})=(7.55\cos(\omega t+0 \text{ rad } -k_1 z) + 2.5\cos(\omega t+0 \text{ rad } +k_1 z))i_x \text{ V/m}$$

In normal incidence, the reflected wave is related to the impinging one via the reflection coefficient:

$E^-(0)=E^+(0) \Gamma$, whose expression is $\Gamma=(\eta_2 - \eta_1)/(\eta_2 + \eta_1)$. With the values computed before, $\Gamma=0.33$.

Thus $\eta_2 = \eta_1 (1+\Gamma)/(1-\Gamma)=748 \Omega$.

In such a lossless medium, $\eta_2=377 \Omega * \text{sqrt}(\mu_r/\epsilon_r)$, from which $\mu_r=8$.

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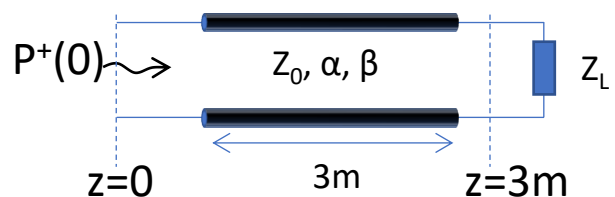
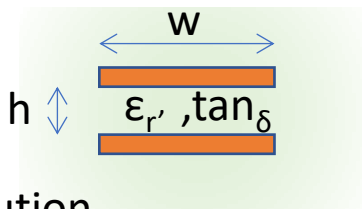
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Solution

The capacitance of a parallel plate capacitor with area $A=w L$ and gap h is C (non p.u.l.)= $\epsilon_0 \epsilon_r A/h$.

The capacitance per unit length of a parallel plate line is hence approximately $C=\epsilon_0 \epsilon_r w/h$.

The quasistatic approximation allows to use this expression also for computations at high frequency such as in the transmission line case we are considering. Therefore $h=\epsilon_0 \epsilon_r w/C=2.2\text{mm}$.

The low-loss approximation ($R \ll \omega L$, $G \ll \omega C$) allows to simplify the computation of the characteristic impedance and of the propagation constant of the line:

$$Z_0 \approx \sqrt{L/C} = 50 \Omega \quad \text{and} \quad \gamma = \sqrt{(j\omega L + R)(j\omega C + G)} \approx j\omega \sqrt{LC} + R/(2Z_0) + GZ_0/2$$

$$\text{From which } \beta = \text{imag}(\gamma) = \omega \sqrt{LC} = 695 \text{ rad/m} \quad \text{and} \quad \alpha = \text{real}(\gamma) = GZ_0/2 = 0.25 \text{ Np/m} = 2.17 \text{ dB/m}$$

The power absorbed by the load can be computed by the difference between the power on the line travelling toward the load and the power on the line travelling back, both evaluated at the load section. However, the condition of $Z_L=Z_0$ implies that the reflection coefficient at the load section is equal to 0.

Hence there is no counter-propagating wave.

Thus the power absorbed by the load is the whole power carried by the forward-propagating wave when it reaches the load.

Since the forward-propagating wave travels as $V^+(z)=V^+(0) e^{-\gamma z}$ (and similarly for the corresponding current), the power carried by the forward propagating wave is

$$P^+(z) = 0.5 \cdot \text{real}(V^+(0) \cdot \text{conj}(I^+(0))) e^{-2\alpha z} = P^+(0) e^{-2\alpha z}$$

The amount of power of the forward-travelling wave reaching the load and thus absorbed by it (with $Z_L=Z_0$) is thus $10\text{W} e^{-2 \cdot 0.25 \text{ Np/m} \cdot 3\text{m}} = 2.23\text{W}$.